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Benchmarking a BI-Population CMA-ES on the BBOB-2009 Noisy Testbed

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ABSTRACT

We benchmark the BI-population CMA-ES on the BBOB-2009 noisy functions testbed. BI-population refers to a multistart strategy with equal budgets for two interlaced restart strategies, one with an increasing population size and one with varying small population sizes. The latter is presumably of little use on a noisy testbed. The BI-population CMA-ES could solve 29, 27 and 26 out of 30 functions in search space dimension 5, 10 and 20 respectively. The time to find the solution ranges between $100D$ and $10^5 D^2$ objective function evaluations, where D is the search space dimension.

Categories and Subject Descriptors

G.1.6 [Numerical Analysis]: Optimization—*global optimization, unconstrained optimization*; F.2.1 [Analysis of Algorithms and Problem Complexity]: Numerical Algorithms and Problems

General Terms

Algorithms

Keywords

Benchmarking, Black-box optimization, Direct search, Evolutionary computation, CMA-ES

1. INTRODUCTION

The *covariance matrix adaptation evolution strategy* (CMA-ES) [2, 6, 7] is a stochastic, population-based search method in continuous search spaces, aiming at minimizing an objective function $f : \mathbb{R}^D \rightarrow \mathbb{R}$ in a black-box scenario. In this paper, the $(\mu/\mu_w, \lambda)$ -CMA-ES is applied in a multistart strategy and benchmarked on 30 noisy functions. The multistart consists of two interlacing strategies, one with increasing population size, the other with varying small population size. The algorithm is given in a complementing paper in the same proceedings [3].

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2. ALGORITHM AND PARAMETER SETTINGS

The algorithm and all parameters are described in [3]. The following parameters have been chosen differently, where λ denotes the offspring population size.

$\text{MaxIter} = 1000 + 500(D + 3)^2/\sqrt{\lambda}$ has been chosen ten times larger, as the noisy functions are expected to be more difficult to solve.

$c_1 = \frac{0.4}{(D+1.3)^2 + \mu_w}$ and $c_\mu = \min\left(1 - c_1, 0.4 \frac{\mu_w - 2 + 1/\mu_w}{(D+2)^2 + \mu_w}\right)$, the learning rates for the covariance matrix have been chosen five times smaller than by default. With default learning rates, the learning of the covariance matrix is the algorithm component that is most susceptible to uncertainties in the selection. Surprisingly, this change did not produce a striking improvement, but slightly more consistent results (e.g. f_{105} , f_{108} and f_{117} are solved also in 40-D).

Restarts are launched until $10^6 D$ function evaluations are exceeded. The stagnation termination criterion

Stagnation: terminate a run, if the median of the 20 newest values is not smaller than the median of the 20 oldest values, respectively, in the two arrays containing the best function values and the median function values of the last $\lceil 0.2t + 120 + 30D/\lambda \rceil$ iterations, where t denotes the iteration counter,

turns out to be crucial for the noisy testbed. Most other standard termination criteria regularly fail. We presume that restarts with small population size are less valuable on a noisy testbed, which leaves yet room for improvement.

The same parameter setting is used for all functions and therefore the crafting effort according to [4] is $\text{CrE} = 0$.

3. SUCCESSFUL POPULATION SIZE

We investigate the population sizes of the final successful runs. In Table 1 minimal, median (the larger in case of even data) and maximal population size are given for 10-D and 20-D. Functions solved with default offspring population size, $\lambda = 10$ and 12, are the sphere function with moderate noise and about half of the functions with Cauchy noise (function numbers in *italics*). Otherwise is the typical population size $10D$ or larger.

Table 2 tabulates minimal, median (the larger in case of even data) and maximal initial step-size σ^0 of the final successful runs, whenever $\sigma^0 < 2$ in at least one successful case.

Table 1: Final, successful population sizes. If less than three successful trials included restarts, only the median (default population size) is given

f	$D = 10$			$D = 20$		
	min	med	max	min	med	max
101		10			12	
102		10			12	
103		10			12	
104	20	20	40	96	96	192
105	40	80	80	192	192	384
106		10			12	
107	20	20	20	24	24	48
108	80	160	160	192	192	384
109		10			12	
110	—	—	—	—	—	—
111	—	—	—	—	—	—
112		10			12	
113	40	80	320	192	384	384
114	160	320	640	286	768	768
115	40	80	160	185	192	384
116	80	160	160	192	384	384
117	160	320	640	768	768	768
118		10			12	
119	160	160	160	384	384	384
120	320	640	1280	1536	1536	1536
121		10			12	
122	80	160	320	384	768	768
123	640	1280	1280	—	—	—
124	40	80	160	96	192	192
125	640	1280	2560	3072	6144	6144
126	—	—	—	—	—	—
127	239	640	1280	384	1536	3072
128	11	40	320	37	192	768
129	80	118	1280	1301	3072	6144
130	10	26	166	12	24	192

Table 2: Initial step-size σ^0 of successful restarts for functions, where $\sigma^0 < 2$ was successful at least once

f	$D = 10$			f	$D = 20$		
	min	med	max		min	med	max
115	0.126	2.0	2.0	114	1.06	2.0	2.0
125	0.72	2.0	2.0	115	0.068	2.0	2.0
127	0.158	2.0	2.0	122	0.2	2.0	2.0
128	0.28	1.8	2.0	128	0.64	1.56	2.0
129	0.8	2.0	2.0	129	1.42	2.0	2.0
130	0.06	0.64	2.0	130	0.042	0.38	2.0

The data neither rule out nor suggest that f_{130} might benefit from a small initial step-size. Overall, as expected, the small initial step-size is of little use and, if anything, rather disadvantageous on the BBOB-2009 noisy testbed.

4. RESULTS AND DISCUSSION

The results of CPU timing experiments are given in [3]: using Matlab, about $2\text{--}3 \times 10^{-4}$ seconds per function evaluation are needed on the BBOB-2009 f_8 function for up to 40-D. Results from the performance experiments according to [4] on the benchmarks functions given in [1, 5] are presented in Figures 1 and 2 and in Tables 3 and 4.

The number of solved functions are 30, 30, 29, 27, 26 and

24 out of 30 functions in 2, 3, 5, 10, 20 and 40-D, respectively.

The typical scaling of the running time (number of function evaluations) is quadratic with the dimension (see Figure 1). With the moderate noise models and with the Cauchy noise model the sphere function can be solved in linear time. More severe noise impairs the scaling behavior by one order of magnitude to quadratic. Similarly, on the Rosenbrock function the severe noise impairs the scaling by one order from roughly quadratic to roughly cubic. Here, the observed failure is presumably due to a too small maximum number of function evaluations allowed.

The expected running times appear rather uniform on the log-scale between $100D$ and $10^5 D^2$ function evaluations (upper figures in Figure 2). The graphs suggest that, in higher dimension, with more function evaluations even more functions can be solved.

Acknowledgments

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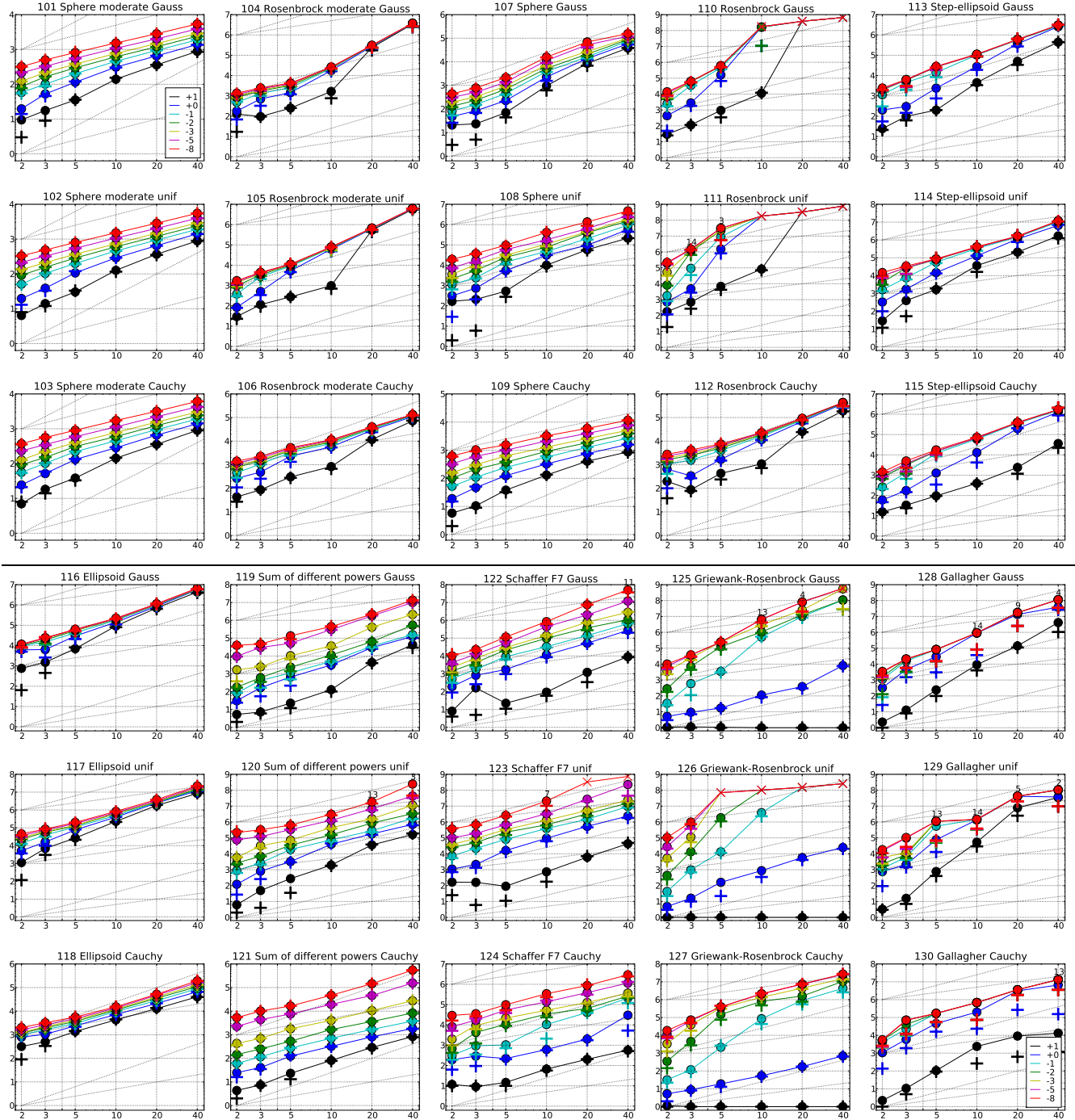


Figure 1: Expected Running Time (ERT, $\bullet$) to reach $f_{\text{opt}} + \Delta f$ and median number of function evaluations of successful trials (+), shown for $\Delta f = 10, 1, 10^{-1}, 10^{-2}, 10^{-3}, 10^{-5}, 10^{-8}$ (the exponent is given in the legend of f_{101} and f_{130}) versus dimension in log-log presentation. The ERT(Δf) equals to $\#FES(\Delta f)$ divided by the number of successful trials, where a trial is successful if $f_{\text{opt}} + \Delta f$ was surpassed during the trial. The $\#FES(\Delta f)$ are the total number of function evaluations while $f_{\text{opt}} + \Delta f$ was not surpassed during the trial from all respective trials (successful and unsuccessful), and f_{opt} denotes the optimal function value. Crosses ($\times$) indicate the total number of function evaluations $\#FES(-\infty)$. Numbers above ERT-symbols indicate the number of successful trials. Annotated numbers on the ordinate are decimal logarithms. Additional grid lines show linear and quadratic scaling.

f_{101} in 5-D, N=15, mFE=930						f_{101} in 20-D, N=15, mFE=3014						f_{102} in 5-D, N=15, mFE=882						f_{102} in 20-D, N=15, mFE=3122					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}		
10	15	3.5e1	2.9e1	4.2e1	3.5e1	15	3.6e2	3.4e2	3.8e2	3.6e2	10	15	3.0e1	2.5e1	3.6e1	3.0e1	15	3.7e2	3.5e2	3.9e2	3.7e2		
1	15	1.1e2	1.0e2	1.2e2	1.1e2	15	6.5e2	6.3e2	6.7e2	6.5e2	1	15	1.1e2	9.6e1	1.2e2	1.1e2	15	6.5e2	6.3e2	6.6e2	6.5e2		
1e-1	15	2.0e2	1.9e2	2.1e2	2.0e2	15	9.4e2	9.2e2	9.5e2	9.4e2	1e-1	15	2.0e2	1.9e2	2.1e2	2.0e2	15	9.4e2	9.2e2	9.6e2	9.4e2		
1e-3	15	3.8e2	3.6e2	3.9e2	3.8e2	15	1.5e3	1.4e3	1.5e3	1.5e3	1e-3	15	3.7e2	3.6e2	3.8e2	3.7e2	15	1.5e3	1.5e3	1.5e3	1.5e3		
1e-5	15	5.6e2	5.4e2	5.7e2	5.6e2	15	2.0e3	2.0e3	2.0e3	2.0e3	1e-5	15	5.4e2	5.3e2	5.6e2	5.4e2	15	2.0e3	2.0e3	2.1e3	2.0e3		
1e-8	15	8.2e2	8.0e2	8.3e2	8.2e2	15	2.8e3	2.8e3	2.9e3	2.8e3	1e-8	15	8.0e2	7.8e2	8.2e2	8.0e2	15	2.9e3	2.8e3	2.9e3	2.9e3		
f_{103} in 5-D, N=15, mFE=994						f_{103} in 20-D, N=15, mFE=3386						f_{104} in 5-D, N=15, mFE=7644						f_{104} in 20-D, N=15, mFE=668758					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}		
10	15	3.8e1	3.0e1	4.7e1	3.8e1	15	3.6e2	3.4e2	3.7e2	3.6e2	10	15	2.5e2	2.4e2	2.7e2	2.5e2	15	2.4e5	2.0e5	2.8e5	2.4e5		
1	15	1.3e2	1.2e2	1.4e2	1.3e2	15	6.6e2	6.4e2	6.7e2	6.6e2	1	15	1.4e3	1.2e3	1.7e3	1.4e3	15	2.8e5	2.3e5	3.3e5	2.8e5		
1e-1	15	2.2e2	2.1e2	2.3e2	2.2e2	15	9.5e2	9.3e2	9.6e2	9.5e2	1e-1	15	2.5e3	2.3e3	2.8e3	2.5e3	15	2.9e5	2.4e5	3.4e5	2.9e5		
1e-3	15	4.0e2	3.9e2	4.1e2	4.0e2	15	1.6e3	1.5e3	1.6e3	1.6e3	1e-3	15	3.5e3	3.3e3	3.8e3	3.5e3	15	3.0e5	2.5e5	3.5e5	3.0e5		
1e-5	15	5.9e2	5.8e2	6.1e2	5.9e2	15	2.2e3	2.2e3	2.2e3	2.2e3	1e-5	15	3.9e3	3.6e3	4.2e3	3.9e3	15	3.0e5	2.5e5	3.5e5	3.0e5		
1e-8	15	9.1e2	8.9e2	9.2e2	9.1e2	15	3.2e3	3.1e3	3.2e3	3.2e3	1e-8	15	4.3e3	4.0e3	4.6e3	4.3e3	15	3.1e5	2.6e5	3.6e5	3.1e5		
f_{105} in 5-D, N=15, mFE=19372						f_{105} in 20-D, N=15, mFE=1.28e6						f_{106} in 5-D, N=15, mFE=11108						f_{106} in 20-D, N=15, mFE=86380					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}		
10	15	2.8e2	2.6e2	2.9e2	2.8e2	15	5.3e5	4.4e5	6.1e5	5.3e5	10	15	3.0e2	2.8e2	3.3e2	3.0e2	15	1.2e4	1.1e4	1.3e4	1.2e4		
1	15	5.2e3	4.4e3	6.2e3	5.2e3	15	6.1e5	5.2e5	7.1e5	6.1e5	1	15	2.3e3	1.6e3	3.0e3	2.3e3	15	2.9e4	2.3e4	3.5e4	2.9e4		
1e-1	15	8.9e3	7.8e3	1.0e4	8.9e3	15	6.3e5	5.3e5	7.3e5	6.3e5	1e-1	15	3.3e3	2.6e3	4.1e3	3.3e3	15	3.3e4	2.7e4	3.9e4	3.3e4		
1e-3	15	1.0e4	9.2e3	1.2e4	1.0e4	15	6.5e5	5.5e5	7.5e5	6.5e5	1e-3	15	4.4e3	3.6e3	5.2e3	4.4e3	15	3.7e4	3.1e4	4.3e4	3.7e4		
1e-5	15	1.1e4	9.7e3	1.2e4	1.1e4	15	6.6e5	5.7e5	7.6e5	6.6e5	1e-5	15	4.8e3	4.0e3	5.6e3	4.8e3	15	3.9e4	3.3e4	4.5e4	3.9e4		
1e-8	15	1.1e4	1.0e4	1.3e4	1.1e4	15	6.8e5	5.8e5	7.8e5	6.8e5	1e-8	15	5.3e3	4.5e3	6.2e3	5.3e3	15	4.0e4	3.5e4	4.6e4	4.0e4		
f_{107} in 5-D, N=15, mFE=3162						f_{107} in 20-D, N=15, mFE=141332						f_{108} in 5-D, N=15, mFE=200594						f_{108} in 20-D, N=15, mFE=3.02e6					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}		
10	15	7.0e1	4.6e1	9.6e1	7.0e1	15	8.6e3	6.9e3	1.0e4	8.6e3	10	15	5.3e2	3.1e2	7.7e2	5.3e2	15	5.8e4	5.1e4	6.5e4	5.8e4		
1	15	2.3e2	1.9e2	2.7e2	2.3e2	15	1.4e4	1.1e4	1.6e4	1.4e4	1	15	5.4e3	4.2e3	6.5e3	5.4e3	15	9.7e4	8.3e4	1.1e5	9.7e4		
1e-1	15	4.5e2	4.0e2	5.1e2	4.5e2	15	1.6e4	1.4e4	1.9e4	1.6e4	1e-1	15	1.4e4	1.2e4	1.8e4	1.4e4	15	2.0e5	1.7e5	2.3e5	2.0e5		
1e-3	15	9.4e2	8.8e2	1.0e3	9.4e2	15	2.7e4	2.4e4	3.0e4	2.7e4	1e-3	15	3.1e4	2.6e4	3.6e4	3.1e4	15	4.5e5	3.9e5	5.0e5	4.5e5		
1e-5	15	1.4e3	1.3e3	1.4e3	1.4e3	15	5.2e4	4.2e4	6.4e4	5.2e4	1e-5	15	5.9e4	5.3e4	6.4e4	5.9e4	15	6.3e5	5.6e5	7.0e5	6.3e5		
1e-8	15	2.2e3	2.0e3	2.3e3	2.2e3	15	6.9e4	5.7e4	8.2e4	6.9e4	1e-8	15	9.7e4	8.3e4	1.1e5	9.7e4	15	1.4e6	1.1e6	1.6e6	1.4e6		
f_{109} in 5-D, N=15, mFE=1922						f_{109} in 20-D, N=15, mFE=6878						f_{110} in 5-D, N=15, mFE=1.33e6						f_{110} in 20-D, N=15, mFE=3.09e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}		
10	15	3.8e1	3.2e1	4.4e1	3.8e1	15	4.1e2	3.8e2	4.3e2	4.1e2	10	15	9.5e2	4.1e2	1.5e3	9.5e2	0	<i>17e+0</i>	<i>16e+0</i>	<i>17e+0</i>	<i>1.8e7</i>		
1	15	1.2e2	1.1e2	1.4e2	1.2e2	15	7.5e2	7.2e2	7.8e2	7.5e2	1	15	1.6e5	9.9e4	2.2e5	1.6e5	.	.	.	.	.		
1e-1	15	2.4e2	2.3e2	2.7e2	2.4e2	15	1.3e3	1.2e3	1.3e3	1.3e3	1e-1	15	4.5e5	3.3e5	5.7e5	4.5e5	.	.	.	.	.		
1e-3	15	6.2e2	5.9e2	6.6e2	6.2e2	15	2.6e3	2.5e3	2.7e3	2.6e3	1e-3	15	5.9e5	4.9e5	7.0e5	5.9e5	.	.	.	.	.		
1e-5	15	1.0e3	9.5e2	1.1e3	1.0e3	15	3.9e3	3.8e3	4.1e3	3.9e3	1e-5	15	6.0e5	5.0e5	7.1e5	6.0e5	.	.	.	.	.		
1e-8	15	1.5e3	1.5e3	1.6e3	1.5e3	15	6.0e3	5.8e3	6.1e3	6.0e3	1e-8	15	6.2e5	5.1e5	7.3e5	6.2e5	.	.	.	.	.		
f_{111} in 5-D, N=15, mFE=1.11e7						f_{111} in 20-D, N=15, mFE=2.51e7						f_{112} in 5-D, N=15, mFE=9378						f_{112} in 20-D, N=15, mFE=187012					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}		
10	15	6.9e3	4.4e3	9.5e3	6.9e3	0	<i>18e+0</i>	<i>17e+0</i>	<i>18e+0</i>	<i>1.8e7</i>	10	15	4.3e2	2.6e2	6.1e2	4.3e2	15	2.6e4	2.4e4	2.7e4	2.6e4		
1	14	1.5e6	9.3e5	2.2e6	1.1e6	.	.	.	.	.	1	15	1.7e3	1.4e3	2.0e3	1.7e3	15	6.9e4	5.6e4	8.1e4	6.9e4		
1e-1	8	8.8e6	6.3e6	1.3e7	4.8e6	.	.	.	.	.	1e-1	15	4.0e3	3.6e3	4.3e3	4.0e3	15	7.9e4	6.7e4	9.1e4	7.9e4		
1e-3	4	2.3e7	1.4e7	5.1e7	5.1e6	.	.	.	.	.	1e-3	15	5.8e3	5.4e3	6.1e3	5.8e3	15	8.6e4	7.4e4	1.0e5	8.6e4		
1e-5	3	3.1e7	1.8e7	8.8e7	6.8e6	.	.	.	.	.	1e-5	15	6.6e3	6.3e3	6.9e3	6.6e3	15	9.0e4	7.7e4	1.0e5	9.0e4		
1e-8	3	3.1e7	1.9e7	9.3e7	7.0e6	.	.	.	.	.	1e-8	15	7.6e3	7.2e3	7.9e3	7.6e3	15	9.3e4	8.0e4	1.1e5	9.3e4		
f_{113} in 5-D, N=15, mFE=86966						f_{113} in 20-D, N=15, mFE=795352						f_{114} in 5-D, N=15, mFE=140043						f_{114} in 20-D, N=15, mFE=2.53e6					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}		
10	15	2.0e2	1.7e2	2.3e2	2.0e2	15	5.0e4	3.7e4	6.3e4	5.0e4	10	15	1.7e3	1.3e3	2.1e3	1.7e3	15	2.1e5	1.8e5	2.4e5	2.1e5		
1	15	2.4e3	1.4e3	3.5e3	2.4e3	15	3.6e5	3.1e5	4.2e5	3.6e5	1	15	1.5e4	1.2e4	1.8e4	1.5e4	15	1.1e6	9.5e5	1.3e6	1.1e6		
1e-1	15	1.4e4	1.0e4	1.9e4	1.4e4	15	5.6e5	5.1e5	6.1e5	5.6e5	1e-1	15	5.6e4	4.7e4	6.7e4	5.6e4	15	1.4e6	1.3e6	1.6e6	1.4e6		
1e-3	15	2.7e4	1.9e4	3.5e4	2.7e4	15	5.9e5	5.3e5	6.4e5	5.9e5	1e-3	15	8.3e4	6.9e4	9.7e4	8.3e4	15	1.6e6	1.4e6	1.8e6	1.6e6		
1e-5	15	2.7e4	1.9e4	3.5e4	2.7e4	15	5.9e5	5.3e5	6.4e5	5.9e5	1e-5	15	8.3e4	6.9e4	9.7e4	8.3e4	15	1.6e6	1.4e6	1.8e6	1.6e6		
1e-8	15	2.8e4	2.1e4	3.6e4	2.8e4	15	6.0e5	5.4e5	6.5e5	6.0e5	1e-8	15	8.7e4	7.2e4	1.0e5	8.7e4	15	1.7e6	1.4e6	1.9e6	1.7e6		
f_{115} in 5-D, N=15, mFE=45496						f_{115} in 20-D, N=15, mFE=678416						f_{116} in 5-D, N=15, mFE=115497						f_{116} in 20-D, N=15, mFE=1.69e6					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}		
10	15	9.6e1	7.9e1	1.1e2	9.6e1	15	2.4e3	1.5e3	3.3e3	2.4e3	10	15	7.0e3	5.3e3	8.7e3	7.0e3	15	7.1e5	5.9e5	8.3e5	7.1e5		
1	15	1.3e3	6.0e2	2.0e3	1.3e3	15	2.0e5	1.5e5	2.4e5	2.0e5	1	15	2.9e4	2.1e4	3.8e4	2.9e4	15	8.6e5	7.5e5	9.7e5	8.6e5		
1e-1	15	1.2e4	8.6e3	1.5e4	1.2e4	15	3.6e5	3.1e5	4.1e5	3.6e5	1e-1	15	4.2e4	3.2e4	5.3e4	4.2e4	1						

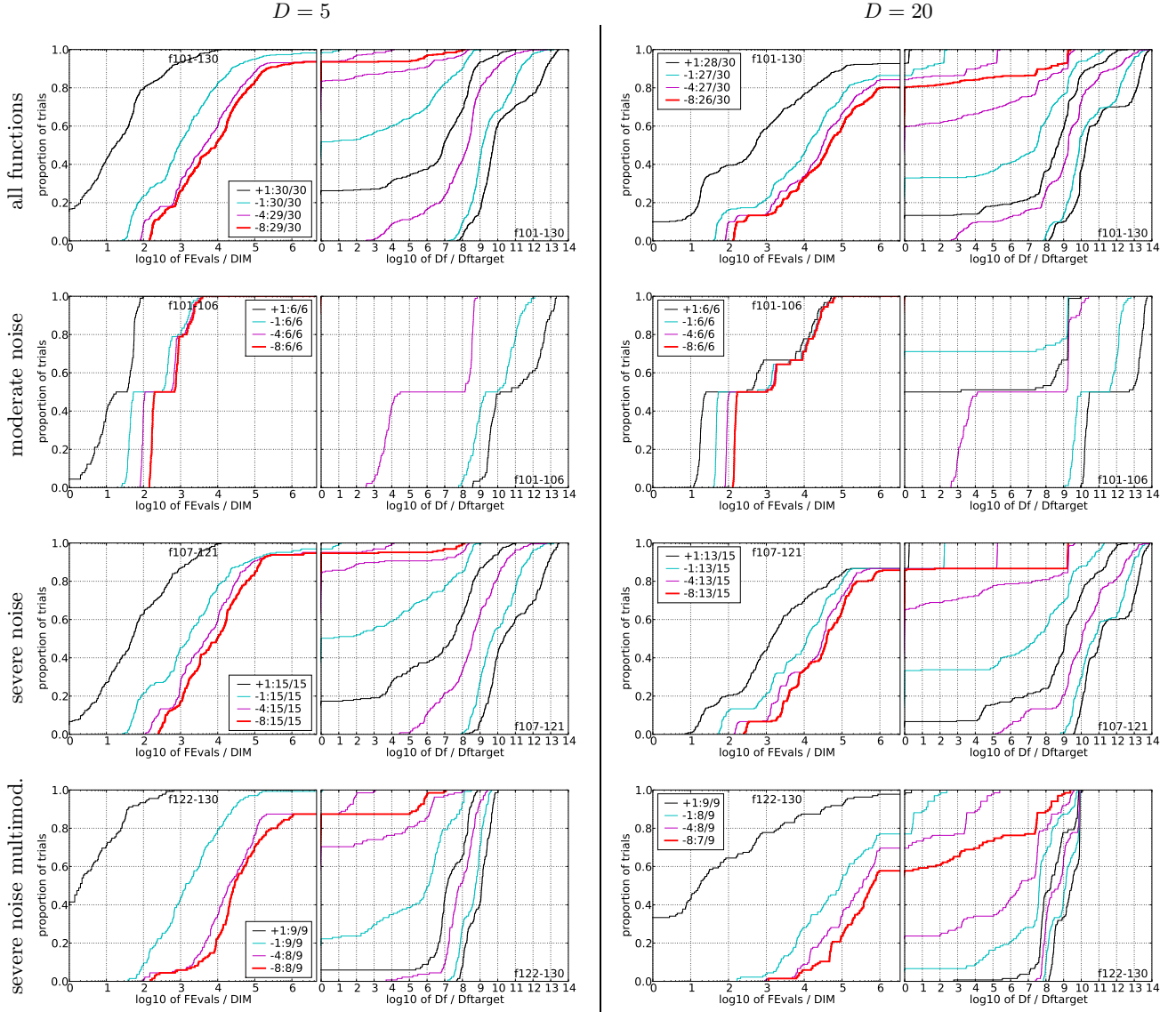


Figure 2: Empirical cumulative distribution functions (ECDFs), plotting the fraction of trials versus running time (left subplots) or versus Δf (right subplots). The thick red line represents the best achieved results. Left subplots: ECDF of the running time (number of function evaluations), divided by search space dimension D , to fall below $f_{\text{opt}} + \Delta f$ with $\Delta f = 10^k$, where k is the first value in the legend. Right subplots: ECDF of the best achieved Δf divided by 10^k (upper left lines in continuation of the left subplot), and best achieved Δf divided by 10^{-8} for running times of $D, 10D, 100D \dots$ function evaluations (from right to left cycling black-cyan-magenta). Top row: all results from all functions; second row: moderate noise functions; third row: severe noise functions; fourth row: severe noise and highly-multimodal functions. The legends indicate the number of functions that were solved in at least one trial. FEvals denotes number of function evaluations, D and DIM denote search space dimension, and Δf and Df denote the difference to the optimal function value.

f_{121} in 5-D, N=15, mFE=17658						f_{121} in 20-D, N=15, mFE=164174					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	2.3e1	1.6e1	3.0e1	2.3e1	15	2.9e2	2.6e2	3.2e2	2.9e2	
1	15	1.2e2	1.1e2	1.4e2	1.2e2	15	8.1e2	7.7e2	8.4e2	8.1e2	
1e-1	15	2.7e2	2.5e2	2.9e2	2.7e2	15	1.7e3	1.6e3	1.8e3	1.7e3	
1e-3	15	1.8e3	1.6e3	2.0e3	1.8e3	15	1.1e4	1.0e4	1.1e4	1.1e4	
1e-5	15	7.6e3	7.3e3	7.9e3	7.6e3	15	4.6e4	4.5e4	4.7e4	4.6e4	
1e-8	15	1.7e4	1.6e4	1.7e4	1.7e4	15	1.5e5	1.4e5	1.5e5	1.5e5	
f_{123} in 5-D, N=15, mFE=5.43e6						f_{123} in 20-D, N=15, mFE=2.56e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	9.1e1	3.5e1	1.6e2	9.1e1	15	6.1e3	4.8e3	7.3e3	6.1e3	
1	15	1.6e4	1.3e4	1.9e4	1.6e4	15	5.3e5	4.2e5	6.4e5	5.3e5	
1e-1	15	8.2e4	6.6e4	9.8e4	8.2e4	15	1.5e6	1.2e6	1.8e6	1.5e6	
1e-3	15	3.4e5	2.8e5	4.0e5	3.4e5	15	5.3e6	4.6e6	6.0e6	5.3e6	
1e-5	15	6.7e5	5.7e5	7.8e5	6.7e5	10	2.7e7	2.3e7	3.4e7	1.9e7	
1e-8	15	2.6e6	2.1e6	3.1e6	2.6e6	0	36e-7	61e-9	16e-6	2.0e7	
f_{125} in 5-D, N=15, mFE=555113						f_{125} in 20-D, N=15, mFE=3.35e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	1.1e0	1.0e0	1.1e0	1.1e0	15	1.0e0	1.0e0	1.0e0	1.0e0	
1	15	1.7e1	1.3e1	2.2e1	1.7e1	15	3.8e2	3.1e2	4.6e2	3.8e2	
1e-1	15	3.4e3	2.6e3	4.4e3	3.4e3	15	9.8e6	8.2e6	1.1e7	9.8e6	
1e-3	15	2.4e5	2.0e5	2.8e5	2.4e5	10	2.5e7	1.9e7	3.4e7	1.5e7	
1e-5	15	2.4e5	2.0e5	2.8e5	2.4e5	4	8.0e7	5.3e7	1.6e8	2.3e7	
1e-8	15	2.5e5	2.1e5	2.9e5	2.5e5	4	8.1e7	5.2e7	1.7e8	2.3e7	
f_{127} in 5-D, N=15, mFE=1.03e6						f_{127} in 20-D, N=15, mFE=1.60e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	1.0e0	1.0e0	1.0e0	1.0e0	15	1.0e0	1.0e0	1.0e0	1.0e0	
1	15	1.9e1	1.3e1	2.5e1	1.9e1	15	1.8e2	1.6e2	1.9e2	1.8e2	
1e-1	15	2.1e3	1.7e3	2.5e3	2.1e3	15	9.0e5	5.9e5	1.2e6	9.0e5	
1e-3	15	3.4e5	2.5e5	4.3e5	3.4e5	15	4.4e6	3.7e6	5.2e6	4.4e6	
1e-5	15	3.9e5	3.0e5	4.8e5	3.9e5	15	7.3e6	6.1e6	8.6e6	7.3e6	
1e-8	15	4.0e5	3.1e5	4.9e5	4.0e5	15	7.5e6	6.2e6	8.8e6	7.5e6	
f_{129} in 5-D, N=15, mFE=6.82e6						f_{129} in 20-D, N=15, mFE=2.27e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	7.7e2	4.8e2	1.1e3	7.7e2	12	7.8e6	5.3e6	1.1e7	7.4e6	
1	15	7.6e4	2.6e4	1.4e5	7.6e4	5	4.1e7	2.6e7	8.0e7	1.3e7	
1e-1	14	5.5e5	5.7e4	1.1e6	5.5e5	5	4.2e7	2.6e7	8.2e7	1.3e7	
1e-3	13	1.1e6	9.5e4	2.0e6	1.1e6	5	4.2e7	2.7e7	8.2e7	1.3e7	
1e-5	13	1.1e6	9.1e4	2.1e6	1.1e6	5	4.2e7	2.6e7	7.8e7	1.3e7	
1e-8	13	1.1e6	9.7e4	2.0e6	1.1e6	5	4.3e7	2.7e7	8.0e7	1.4e7	
f_{122} in 5-D, N=15, mFE=226165						f_{122} in 20-D, N=15, mFE=1.55e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	2.2e1	1.2e1	3.3e1	2.2e1	15	1.2e3	4.7e2	2.0e3	1.2e3	
1	15	1.7e3	1.3e3	2.2e3	1.7e3	15	5.2e4	4.5e4	5.9e4	5.2e4	
1e-1	15	9.2e3	7.1e3	1.1e4	9.2e3	15	1.4e5	1.2e5	1.6e5	1.4e5	
1e-3	15	3.0e4	2.6e4	3.4e4	3.0e4	15	7.9e5	6.5e5	9.5e5	7.9e5	
1e-5	15	5.4e4	4.6e4	6.1e4	5.4e4	15	2.0e6	1.8e6	2.2e6	2.0e6	
1e-8	15	1.2e5	1.0e5	1.3e5	1.2e5	15	7.5e6	6.2e6	8.9e6	7.5e6	
f_{124} in 5-D, N=15, mFE=403943						f_{124} in 20-D, N=15, mFE=1.12e6					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	1.5e1	1.1e1	1.9e1	1.5e1	15	2.0e2	1.8e2	2.3e2	2.0e2	
1	15	2.2e2	2.0e2	2.4e2	2.2e2	15	2.0e3	1.7e3	2.3e3	2.0e3	
1e-1	15	1.0e3	7.3e2	1.4e3	1.0e3	15	4.1e4	3.2e4	5.0e4	4.1e4	
1e-3	15	2.2e4	1.7e4	2.6e4	2.2e4	15	1.3e5	1.1e5	1.5e5	1.3e5	
1e-5	15	5.4e4	4.5e4	6.5e4	5.4e4	15	3.9e5	3.1e5	4.7e5	3.9e5	
1e-8	15	9.8e4	7.0e4	1.3e5	9.8e4	15	8.7e5	7.8e5	9.6e5	8.7e5	
f_{126} in 5-D, N=15, mFE=6.03e6						f_{126} in 20-D, N=15, mFE=1.24e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	1.0e0	1.0e0	1.0e0	1.0e0	15	1.0e0	1.0e0	1.0e0	1.0e0	
1	15	1.6e2	4.0e1	2.8e2	1.6e2	15	5.8e3	4.6e3	6.9e3	5.8e3	
1e-1	15	1.3e4	1.0e4	1.6e4	1.3e4	0	30e-2	24e-2	32e-2	5.6e6	
1e-3	0	67e-4	13e-4	98e-4	2.8e6	.	.	.	.	.	
1e-5	.	.	.	.	.	.	.	.	.	.	
1e-8	.	.	.	.	.	.	.	.	.	.	
f_{128} in 5-D, N=15, mFE=666537						f_{128} in 20-D, N=15, mFE=2.37e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	2.4e2	9.4e1	3.9e2	2.4e2	15	1.4e5	8.7e4	2.0e5	1.4e5	
1	15	2.9e4	8.9e3	5.5e4	2.9e4	10	1.3e7	8.2e6	2.0e7	8.9e6	
1e-1	15	8.2e4	2.8e4	1.4e5	8.2e4	9	1.7e7	1.1e7	2.5e7	1.2e7	
1e-3	15	8.2e4	2.8e4	1.4e5	8.2e4	9	1.7e7	1.2e7	2.5e7	1.2e7	
1e-5	15	8.2e4	2.8e4	1.4e5	8.2e4	9	1.7e7	1.1e7	2.5e7	1.2e7	
1e-8	15	8.3e4	2.8e4	1.4e5	8.3e4	9	1.7e7	1.2e7	2.6e7	1.2e7	
f_{130} in 5-D, N=15, mFE=808354						f_{130} in 20-D, N=15, mFE=1.62e7					
Δf	#	ERT	10%	90%	RT _{succ}	#	ERT	10%	90%	RT _{succ}	
10	15	1.1e2	8.8e1	1.2e2	1.1e2	15	9.1e3	4.2e3	1.4e4	9.1e3	
1	15	4.6e4	2.4e4	7.0e4	4.6e4	15	3.1e6	1.5e6	5.1e6	3.1e6	
1e-1	15	1.7e5	9.7e4	2.4e5	1.7e5	15	3.6e6	1.8e6	5.3e6	3.6e6	
1e-3	15	1.7e5	9.4e4	2.4e5	1.7e5	15	3.6e6	1.9e6	5.3e6	3.6e6	
1e-5	15	1.7e5	9.4e4	2.5e5	1.7e5	15	3.6e6	2.0e6	5.4e6	3.6e6	
1e-8	15	1.7e5	9.7e4	2.5e5	1.7e5	15	3.6e6	1.9e6	5.4e6	3.6e6	

Table 4: Shown are, for functions f_{121} - f_{130} and for a given target difference to the optimal function value Δf : the number of successful trials (#); the expected running time to surpass $f_{\text{opt}} + \Delta f$ (ERT, see Figure 1); the 10%-tile and 90%-tile of the bootstrap distribution of ERT; the average number of function evaluations in successful trials or, if none was successful, as last entry the median number of function evaluations to reach the best function value (RT_{succ}). If $f_{\text{opt}} + \Delta f$ was never reached, figures in *italics* denote the best achieved Δf -value of the median trial and the 10% and 90%-tile trial. Furthermore, N denotes the number of trials, and mFE denotes the maximum of number of function evaluations executed in one trial. See Figure 1 for the names of functions.